براي دسترسي به نسخه كامل حل المسائل، روى لينك زير كليك كنيد و يا به وبسايت "ايبوك ياب" مراجعه بفر ماييد

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Problem 1.1

Given points $P_1(1, -1, 2)$ and $P_2(1, 0, -3)$

(a) Computation of the unit vector in the direction of $\overline{P_1P_2}$

The position vectors of points P_1 and P_2 are

According to the parallelogram rule the vector $\vec{P_1P_2}$ is obtained as follows $\vec{P_1P_2} = \vec{OP_2} - \vec{OP_1} = \underline{i_2} - 5\underline{i_3}$

The unit vector in the direction of $\overline{P_1P_2}$ is

$$\frac{1}{12} = \frac{P_1P_2}{P_1P_2} = \frac{1}{12} - \frac{5}{12} - \frac{5}{12}$$

(b) Computation of the angle $< P_1 OP_2$

The dot product of the vectors \overrightarrow{OP}_1 and \overrightarrow{OP}_2 is $(\overrightarrow{OP}_1)(\overrightarrow{OP}_2) = 1 - 6 = 5$

We have also that

0=130.2

and

$$\cos \Theta = \frac{-5}{160} = -0.6454$$

or

Computation of the angle
$$\langle OP_1P_2 \rangle$$

The vectors $\overrightarrow{P_1O}$ and $\overrightarrow{P_1P_2}$ are
 $\overrightarrow{P_1O} = -\underline{i}_1 + \underline{i}_2 - 2\underline{i}_3$
 $\overrightarrow{P_1P_2} = \underline{i}_2 - 5\underline{i}_3$
Their dot product is

$$(\bar{P},\bar{O})(\bar{P},\bar{P}_{2}) = 1 + 10 = 11$$

We have also that

and

or

$$\cos \phi = \frac{11}{(6)(126)} = 0.8807$$

 $\phi = 28.3^{\circ}$

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(c) Computation of the unit vector in normal to the plane specified by the points O, P1

and
$$P_2$$
.
 $\vec{OP}_1 = \underline{i}_1 - \underline{i}_2 + 2\underline{i}_3$
 $\vec{OP}_2 = \underline{i}_1 - 3\underline{i}_3$

The cross product of these vectors is

$$(\vec{0P}_1) \times (\vec{0P}_2) = (3+0)i_1 + (2+3)i_2 + (0+1)i_3 = 3i_1 + 5i_2 + i_3$$

and

$$i_{\eta} = \pm \frac{3i_1 + 5i_2 + i_3}{135}$$

(d) Computation of the volume of the parallelepiped whose edges are OP1, OP2 and

OP₃.

$$\begin{array}{c}
0P_1 = \underline{i}_1 - \underline{i}_2 + 2\underline{i}_3 \\
0P_2 = \underline{i}_1 - 3\underline{i}_3 \\
0P_3 = -\underline{i}_1 + 2\underline{i}_2 + \underline{i}_3
\end{array}$$

As shown above

$$(\vec{0}\vec{P}_1) \times (\vec{0}\vec{P}_2) = 3\underline{i}_1 + 5\underline{i}_2 + \underline{i}_3$$

And the volume V of the parallelepiped is $V = (\overline{OP}_3) [(\overline{OP}_1) \times (\overline{OP}_2)] = -3 + 10 + 1 = 8 \pi \sqrt{3}$

Problem 1.2

Referring to relation (1.31) we have $\alpha'_1 = \sum_{j=1}^3 \lambda_{ij} \alpha_j = \lambda_{i_1} \alpha_1 + \lambda_{i_2} \alpha_2$ Thus, $\alpha'_1 = \lambda_{11} \alpha_1 + \lambda_{12} \alpha_2 = \alpha_1 = 4$ $\alpha'_2 = \lambda_{21} \alpha_1 + \lambda_{22} \alpha_2 = \frac{\alpha_2}{12} = \frac{3}{12}$ $\alpha'_3 = \lambda_{31} \alpha_1 + \lambda_{32} \alpha_2 = \frac{-\alpha_2}{12} = -\frac{3}{12}$

or

$$A = 4_{\frac{1}{3}} + \frac{3}{12} \frac{1}{12} - \frac{3}{12} \frac{1}{13} = 4_{\frac{1}{2}1} + \left(\frac{3}{2}\right)_{\frac{1}{2}2} - \left(\frac{3}{2}\right)_{\frac{1}{2}3}$$

Another way of solving this problem is referring to relation (1.33a)

$$\begin{pmatrix} a_1' \\ a_2' \\ a_3' \end{pmatrix} = \begin{bmatrix} 1 & 0 & 0 \\ 0 & \frac{1}{12} & \frac{1}{12} \\ 0 & \frac{-1}{12} & \frac{1}{12} \end{bmatrix} \begin{pmatrix} 4 \\ 3 \\ 0 \end{pmatrix} = \begin{pmatrix} 4 \\ 3 \\ \frac{1}{12} \\ -\frac{3}{12} \\ \frac{1}{12} \end{pmatrix}$$

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Problem 1.3

or

(a) Calculation of the angle between the vectors \mathbf{a} and \mathbf{b} . We denote this angle by $\boldsymbol{\Theta}$

$$\cos \Theta = \frac{\underline{8} \cdot \underline{9}}{1 \underline{2} | \underline{19} |} = \frac{\underline{12 + 8 - 12}}{\underline{129} | \underline{56} |} = \frac{\underline{8}}{\underline{129} | \underline{56} |} = 0.1985$$

$$\Theta = \overline{78.55^{\circ}}$$

(b) The component of the vector \mathbf{b} in the direction of vector \mathbf{a} is given by the following dot product

$$b \cdot \frac{a}{181} = \frac{8}{129} = 1.49m$$

(c) We calculate the cross product of the vectors **a** and **b** referring to relation (1.19) $g_{1} \underbrace{b}_{2} = (24+4) \underbrace{i}_{1} + (8+18) \underbrace{i}_{2} + (-6+16) \underbrace{i}_{3} = 28 \underbrace{i}_{1} + 26 \underbrace{i}_{2} + 10 \underbrace{i}_{3}$

The area of the parallelogram whose sides are the vectors a and b is equal to the

magnitude of the vector (**a** x **b**), thus $|(\underline{a} \times \underline{b})| = |\underline{28^2 + 26^2 + 10^2} = 39.5 \text{ m}^2$

(d) The volume of the parallelepiped specified by the vectors **a**, **b** and **c** is equal to the

absolute value of the dot product of the vectors c and (a x b), thus

Problem 1.4



The position vectors of points A, B and P are $\underline{r}_A = -2\underline{i}_1 + \underline{i}_2 + 3\underline{i}_3$ $\underline{r}_B = -\underline{i}_1 + 2\underline{i}_2 - \underline{i}_3$

10= -11+212-1 1p= -11+212 https://ebookyab.ir/solution-manual-advanced-mechanics-of-materials-and-applied-elasticity-armenakas/ Email: ebookyab@m@gmail.com, Phone:+989359542944 (Telegram, WhatsApp, Eitaa)

And the vector
$$\overrightarrow{AB}$$
 is
 $\overrightarrow{AB} = \overrightarrow{B} - \overrightarrow{A} = \overrightarrow{1}_1 + \overrightarrow{1}_2 - 4 \overrightarrow{1}_3$

The unit vector in the direction of the vector \overrightarrow{AB} is

Referring to Fig. a the shortest distance from point P to the line passing through points A and B is equal to the magnitude of the vector PC. Thus,

(a)

where

Thus,

$$\overrightarrow{AP} = \underline{\Gamma}P - \underline{\Gamma}_{A} = -\underline{i}_{1} + 2\underline{i}_{2} + 2\underline{i}_{1} - \underline{i}_{2} - 3\underline{i}_{3} = \underline{i}_{1} + \underline{i}_{2} - 3\underline{i}_{3}$$

We have also that

$$|\vec{PC}| = |\vec{I}AB \times \vec{AP}|$$

$$(\vec{h}AB \times \vec{AP} = \frac{(\vec{h}1 + \vec{h}2 - 4\vec{h}3)}{|\vec{I}B|} \times (\vec{h}1 + \vec{h}2 - 3\vec{h}3) = \frac{1}{|\vec{I}B|} [(-3+4)\vec{h}1 + (-4+3)\vec{h}2 + (1-1)\vec{h}3]$$

$$(\vec{h}AB \times \vec{AP} = \frac{(\vec{h}1 + \vec{h}2 - 4\vec{h}3)}{|\vec{I}B|} \times (\vec{h}1 + \vec{h}2 - 3\vec{h}3) = \frac{1}{|\vec{I}B|} [(-3+4)\vec{h}1 + (-4+3)\vec{h}2 + (1-1)\vec{h}3]$$

 $= \frac{i}{\sqrt{18}} \left(\underline{i}_1 - \underline{i}_2 \right)$ And the magnitude of the vector ($i_{AB} \times AP$) is

$$|i_{AB} \times \overline{AP}| = \left|\frac{2}{18} = \frac{1}{3}\right|$$
 (c)

Substituting relation (c) into (b) we have

Problem 1.5

(a) Referring to relations (1.25a) we have

$$\lambda_{11} \lambda_{13} + \lambda_{21} \lambda_{23} + \lambda_{31} \lambda_{33} = 0$$

 $\lambda_{12} \lambda_{13} + \lambda_{22} \lambda_{23} + \lambda_{32} \lambda_{33} = 0$
 $\lambda_{13}^{2} + \lambda_{23}^{2} + \lambda_{33}^{2} = 1$
(a)

From the data of the problem we have

$$\lambda_{11} = 0$$
 $\lambda_{12} = -\frac{4}{5}$ $\lambda_{13} = \frac{3}{5}$
 $\lambda_{21} = 1$ $\lambda_{22} = 0$ $\lambda_{23} = 0$ (b)

Substituting (b) into (a) we obtain

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$$\lambda_{31} \lambda_{33} = 0$$

$$\left(-\frac{4}{5}\right) \left(\frac{3}{5}\right) + \lambda_{32} \lambda_{33} = 0$$

$$\left(\frac{3}{5}\right)^2 + \lambda_{33}^2 = 1$$

or

$$\lambda_{33} = \pm \frac{4}{5}$$
, $\lambda_{31} = 0$, $\lambda_{32} = \pm \frac{3}{5}$

(b) We denote the given tensor by [A]. Referring to relation (1.37a) we have

$$\begin{bmatrix} A \end{bmatrix} = \begin{bmatrix} A \end{bmatrix} \begin{bmatrix} A \end{bmatrix} \begin{bmatrix} A \end{bmatrix}^{\mathsf{T}} = \begin{bmatrix} 2 & 0 & 0 \\ 0 & 3 & 5 \\ 1 & 0 & 0 \\ 0 & 3 & 5 & 5 \end{bmatrix} \begin{bmatrix} 2 & 0 & 0 \\ 0 & 3 & -5 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 0 & 1 & 0 \\ -\frac{4}{5} & 0 & \frac{3}{5} \\ \frac{3}{5} & 0 & \frac{4}{5} \end{bmatrix} = \begin{bmatrix} \frac{117}{25} & 0 & \frac{56}{25} \\ 0 & 2 & 0 \\ -\frac{69}{25} & 0 & -\frac{13}{25} \end{bmatrix} = \begin{bmatrix} 4.68 & 0 & 2.24 \\ 0 & 2 & 0 \\ -2.16 & 0 & -0.68 \end{bmatrix}$$

Problem 1.6

(a) The coordinates of point P with respect to the system of axes x_1', x_2', x_3' are $\begin{cases}
x_1' \\
x_2' \\
x_3'
\end{cases} = \begin{bmatrix}
\frac{1}{r_2} & -\frac{3}{5r_2} & -\frac{4}{5r_2} \\
0 & \frac{4}{5} & -\frac{3}{5} \\
\frac{1}{r_2} & \frac{3}{5r_2} & \frac{7}{5r_2}
\end{bmatrix} \begin{cases}
-2 \\
1 \\
0
\end{cases} = \begin{cases}
-\frac{13}{5r_2} \\
\frac{4}{5} \\
-\frac{3}{5r_2}
\end{bmatrix} = \begin{cases}
-1.84 \\
0.8 \\
-0.99
\end{cases}$ (b) Expanding relation (1.70) we obtain

$$A_{ij}^{\prime} = \sum_{k=1}^{3} \sum_{m=1}^{3} \lambda_{ik} \lambda_{jm} A_{km} = \sum_{k=1}^{3} (\lambda_{ik} \lambda_{ji} A_{k1} + \lambda_{ik} \lambda_{j2} A_{k2} + \lambda_{ik} \lambda_{j3} A_{k3})$$
$$= \lambda_{i_1} \lambda_{j_2} A_{12} + \lambda_{i_2} \lambda_{j2} A_{22} + \lambda_{i_3} \lambda_{j_2} A_{32}$$

Thus substituting the given values in this equation we have

$$A'_{11} = (\lambda_{11} \lambda_{12}) A_{12} + \lambda'_{12} A_{22} + (\lambda_{13} \lambda_{12}) A_{32}$$

= $-\frac{3}{5} - \frac{9}{50} - \frac{24}{50} = -\frac{63}{50} = -1.26$

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$$A_{12} = (\lambda_{11} \lambda_{22}) A_{12} + (\lambda_{12} \lambda_{22}) A_{22} + (\lambda_{13} \lambda_{22}) A_{32}$$

$$= \frac{B}{512} + \frac{12}{2502} + \frac{32}{2502} = \frac{84}{2502} = 2.336$$

$$A_{13} = (\lambda_{11} \lambda_{32}) A_{12} + (\lambda_{12} \lambda_{32}) A_{22} + (\lambda_{13} \lambda_{32}) A_{32}$$

$$= \frac{3}{5} + \frac{9}{50} + \frac{24}{50} = \frac{63}{50} = 1.260$$

$$A_{21} = (\lambda_{22} \lambda_{12}) A_{22} + (\lambda_{23} \lambda_{12}) A_{32}$$

$$= \frac{12}{2502} - \frac{18}{2502} = \frac{-6}{2502} = -0.170$$

$$A_{22} = \lambda_{22}^{2} A_{22} + (\lambda_{23} \lambda_{22}) A_{32}$$

$$= -\frac{16}{25} + \frac{24}{25} = \frac{8}{25} = 0.320$$

$$A_{23}^{\prime} = (\lambda_{22} \lambda_{32}) A_{22} + (\lambda_{23} \lambda_{32}) A_{32}$$

$$= -\frac{12}{2502} + \frac{18}{2502} = \frac{6}{2502} = 0.170$$

$$A_{31}^{\prime} = (\lambda_{31} \lambda_{12}) A_{12} + (\lambda_{32} \lambda_{12}) A_{22} + (\lambda_{33} \lambda_{12}) A_{32}$$

$$= -\frac{3}{5} + \frac{9}{50} + \frac{24}{50} = \frac{3}{50} = 0.06$$

$$A_{32} = (\lambda_{31} \lambda_{22}) A_{12} + (\lambda_{32} \lambda_{22}) A_{22} + (\lambda_{33} \lambda_{32}) A_{32}$$

$$= \frac{8}{50} + \frac{-12}{2502} - \frac{32}{2502} = -0.113$$

$$A_{33}^{\prime} = (\lambda_{31} \lambda_{32}) A_{12} + (\lambda_{32} \lambda_{32}) A_{22} + (\lambda_{33} \lambda_{32}) A_{32}$$

$$= \frac{3}{5} - \frac{9}{50} - \frac{24}{50} = -\frac{3}{50} = -0.06$$

The same results may be obtained using matrix multiplication. That is

$$\begin{bmatrix} A' \end{bmatrix} = \begin{bmatrix} \frac{1}{12} & \frac{-3}{512} & \frac{-4}{512} \\ 0 & \frac{4}{5} & \frac{-3}{5} \\ \frac{1}{12} & \frac{-3}{512} & \frac{-4}{512} \\ 0 & -1 & 0 \\ 0 & -1 & 0 \\ 0 & -2 & 0 \end{bmatrix} \begin{bmatrix} \frac{1}{12} & 0 & \frac{1}{12} \\ \frac{-3}{512} & \frac{4}{5} & \frac{3}{512} \\ \frac{-4}{512} & \frac{-3}{5} & \frac{4}{512} \\ \frac{-4}{512} & \frac{-3}{5} & \frac{4}{512} \\ \frac{-4}{512} & \frac{-3}{5} & \frac{4}{512} \\ \frac{-4}{512} & \frac{-3}{5} & \frac{5}{512} \\ \frac{-126}{512} & \frac{-3}{55} & \frac{6}{5512} \\ \frac{-126}{512} & \frac{2376}{5512} & \frac{126}{5512} \\ \frac{-126}{5512} & \frac{2376}{5512} & \frac{126}{5512} \\ \frac{-3}{50} & \frac{-4}{2512} & \frac{-3}{50} \\ \frac{-0.16}{500} & -0.113 & -0.06 \\ \frac{-0.13}{500} & -0.06 \\ \frac{-0.13}{50} & -0.06 \\ \frac{-0.13$$

(c) The equation of the plane $x_1-x_2+2x_3 = 1$ can be rewritten as

$$\begin{bmatrix} 1 & -1 & 2 \end{bmatrix} \begin{pmatrix} x_1 \\ x_2 \\ x_3 \end{pmatrix} = 1$$
 (a)

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Referring to the equation (1.34a) we have

$$\begin{pmatrix} x_{1} \\ x_{2} \\ x_{3} \end{pmatrix} = \begin{bmatrix} \Lambda_{5} \end{bmatrix}^{T} \begin{cases} x_{1}' \\ x_{2}' \\ x_{3}' \end{cases} = \begin{bmatrix} \frac{1}{r_{2}} & 0 & \frac{1}{r_{2}} \\ \frac{-3}{5r_{2}} & \frac{4}{5} & \frac{3}{5r_{2}} \\ \frac{-4}{5r_{2}} & \frac{-3}{5} & \frac{4}{5r_{2}} \\ \frac{-3}{5r_{2}} & \frac{4}{5} & \frac{3}{5r_{2}} \\ \frac{-4}{5r_{2}} & \frac{-3}{5} & \frac{4}{5r_{2}} \\ \frac{-2}{5} & \frac{4}{5r_{2}} & \frac{1}{5r_{2}} \\ \frac{-2}{5} & \frac{4}{5r_{2}} & \frac{1}{5r_{2}} \\ \frac{-2}{5} & \frac{4}{5r_{2}} & \frac{1}{5r_{2}} \\ \frac{-2}{5r_{2}} & \frac{1}{5r_{2}} \\ \frac{-2}{5r$$

Problem 1.7

(a) Referring to relation (1.33a) the coordinates of point P in the system of axes x_i' are

$$\begin{cases} x_{1}' \\ x_{2}' \\ x_{3}' \end{cases} = \begin{bmatrix} \Lambda_{5} \end{bmatrix} \begin{cases} x_{1} \\ x_{2} \\ x_{3} \end{cases} = \begin{bmatrix} \frac{1}{r_{5}} & 0 & -\frac{2}{r_{6}} \\ \frac{1}{r_{5}} & \frac{1}{r_{5}} & \frac{1}{r_{6}} \\ \frac{1}{r_{5}} & \frac{1}{r_{5}} & \frac{1}{r_{6}} \\ \frac{1}{r_{5}} & -\frac{1}{r_{6}} \\ \frac{1}{r_{5}} & -\frac{1}{r_{6}} \\ \frac{1}{r_{5}} & -\frac{1}{r_{6}} \\ \frac{1}{r_{6}} & \frac{1}{r_{6}} \\ \frac{3r_{5}+2r_{5}-4}{r_{6}} \\ \frac{3r_{5}+2r_{5}-4}{r_{6}} \\ \frac{3r_{5}-2r_{5}-4}{r_{6}} \\ \frac{1}{r_{6}} & -1,315 \end{bmatrix}$$

(b) Referring to equation (1.73b) we have $[A'] = [A_s] [A] [A_s]^T$

Thus,

$$\begin{bmatrix} A' \end{bmatrix} = \begin{bmatrix} \frac{1}{13} & 0 & -\frac{2}{16} \\ \frac{1}{13} & \frac{1}{12} & \frac{1}{16} \\ \frac{1}{13} & \frac{1}{12} & \frac{1}{12} \\ \frac{1}{16} & \frac{1}{16} \\ \frac{1}{16} & \frac{1}{16} \\ \frac{1}{16} & \frac{1}{16} \\ \frac{1}{16} & \frac{1}{16} \\ \frac{1}{13} & \frac{1}{13} \\ \frac{1}$$

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(c) The equation of the plane in the system of axes
$$x_1$$
, x_2 , x_3 is

2x1+3x2-x3=1

or

$$\begin{bmatrix} 2 & 3 & -1 \end{bmatrix} \begin{cases} x_1 \\ x_2 \\ x_3 \end{cases} = 1$$
 (a)

From relation (1.34a) we have

$$\begin{cases} x_{1} \\ x_{2} \\ x_{3} \\ x_{2} \\ x_{2} \\ x_{3} \\ x_{2} \\ x_{2} \\ x_{3} \\ x_{2} \\ x_{3} \\ x_{2} \\ x_{3} \\ x_{4} \\ x_{5} \\ x_{6} \\ x_{6} \\ x_{6} \\ x_{6} \\ x_{6} \\ x_{3} \\ x_{6} \\ x_{3} \\ x_{6} \\ x_{3} \\ x_{6} \\ x_{3} \\ x_{5} \\ x_{6} \\ x_{3} \\ x_{5} \\ x$$

Substituting equation (b) into (a) we have

$$\begin{bmatrix} 2 & 3 & -1 \end{bmatrix} \begin{bmatrix} \frac{4}{13} & \frac{1}{13} & \frac{1}{13} & \frac{1}{13} \\ 0 & \frac{1}{12} & -\frac{1}{12} \\ -\frac{2}{16} & \frac{1}{16} & \frac{1}{16} \end{bmatrix} \begin{cases} x_1' \\ x_2' \\ x_3' \end{cases} = 1$$

Or

Problem 1.8A

Given the symmetric tensor of the second rank

$$[A] = \begin{bmatrix} 2 & i & 0 \\ i & 4 & 0 \\ 0 & 0 & 3 \end{bmatrix}$$

(a) Referring to relation (1.124) we have the following stationary values for the tensor[A]

$$\widetilde{A}_{1} = \frac{1}{2} (A_{11} + A_{22}) + \sqrt{\left(\frac{A_{11} - A_{22}}{2}\right)^{2} + A_{12}^{2}} = 3 + 12$$

$$\widetilde{A}_{2} = \frac{1}{2} (A_{11} + A_{22}) - \sqrt{\left(\frac{A_{11} - A_{22}}{2}\right)^{2} + A_{12}^{2}} = 3 - \sqrt{2}$$

$$\widetilde{A}_{3} = 3$$

From relation (1.122) we have

$$\tan 2\bar{\phi}_{11} = \frac{2A_{12}}{A_{11} - A_{22}} = -1$$
 and $2\bar{\phi}_{11} = 135^{\circ}$

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> φ̃₌ 67.5° counter-clockwise In Figure a. we show the principal axes \tilde{x}_1, \tilde{x}_2 Axis of maximum X₂ diagonal component х Х, X Axes of maximum non-diagonal component ~ x2 = 22.5° **φ**∥=67.5°-×,

(b) Referring to relation (1.129) the maximum value of the non-diagonal components of the tensor [A] is

$$(A'_{12})_{\max} = \left[\left(\frac{A_{11} - A_{12}}{2} \right)^2 + A_{12}^2 \right]^{\frac{1}{2}} = \left[\left(\frac{2-4}{2} \right)^2 + \frac{1}{2} \right]^{\frac{1}{2}} = \sqrt{2}$$

From relation (1.127) we have

$$\tan 2\tilde{\tilde{\phi}}_{11} = -\frac{A_{11}-A_{22}}{2A_{12}} = -\frac{2-4}{2} = 1$$
 and $2\tilde{\tilde{\phi}}_{11} = 45^{\circ}$

Or

Or

$$\tilde{\tilde{\phi}}_{ij}$$
 = 22.5° counter-clockwise

In Fig. a we also show the axes $\tilde{\tilde{x}}_1, \tilde{\tilde{x}}_2$ with respect of which this maximum value of the non-diagonal components occurs.

(c) Referring to relation (1.61) the diagonal component of the tensor [A] in the direction of the unit vector in is 7 517

$$A_{nn} = \{n\}^{T} [A] \{n\} = \frac{1}{13} [1 (-1)] \begin{bmatrix} 2 & 1 & 0 \\ 1 & 4 & 0 \\ 0 & 0 & 3 \end{bmatrix} \begin{bmatrix} 1 & 1 \\ -1 \\ -1 \end{bmatrix} \frac{1}{13} = \frac{11}{3}$$

Problem 1.8B

Given the symmetric tensor of the second rank

$$\begin{bmatrix} B \end{bmatrix} = \begin{bmatrix} 0 & 0 & 0 \\ 0 & 3 & -1 \\ 0 & -1 & 2 \end{bmatrix}$$

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(a) Referring to relation (1.124) we have the following stationary values for the tensor [B]

$$B_{1}=0$$

$$\tilde{B}_{2}=\frac{1}{2}(B_{22}+B_{33})+\sqrt{\left(\frac{B_{22}-B_{33}}{2}\right)^{2}+B_{23}^{2}}=\frac{5+15}{2}$$

$$\tilde{B}_{3}=\frac{1}{2}(B_{22}+B_{33})-\sqrt{\left(\frac{B_{22}-B_{33}}{2}\right)^{2}+B_{23}^{2}}=\frac{5-15}{2}$$

From relation (1.122) we have

$$tan_{2\phi_{22}} = \frac{2B_{23}}{B_{22}} = \frac{-2}{3-2} = -2$$
 and $2\phi_{22} = -63.43^{\circ}$

Or

 $\tilde{\Phi}_{22} = 31.72^\circ$ clockwise

In Figure a we show the principal axes \tilde{x}_2 , \tilde{x}_3





(b) Referring to relation (1.129) the maximum value of the non-diagonal components of the tensor [B] is

$$(B'_{23})_{mox} = \left[\left(\frac{B_{22} - B_{33}}{2} \right)^2 + B_{23}^2 \right]^{1/2} = \left[\left(\frac{3 - 2}{2} \right)^2 + (-1)^2 \right]^{1/2} = \frac{15}{2}$$

From relation (1.127) we have

$$\tan 2\tilde{\phi}_{22} = -\frac{B_{21}-B_{33}}{2B_{23}} = -\frac{3-2}{(-2)} = \frac{1}{2}$$
 and $2\tilde{\phi}_{22} = 26.56^{\circ}$

Or

 $\overline{\Phi}_{22} = 13.28$ counter-clockwise In Fig. a we also show the axes \tilde{x}_2 and \tilde{x}_3 with respect of which this maximum value of the non-diagonal components occurs. https://ebookyab.ir/solution-manual-advanced-mechanics-of-materials-and-applied-elasticity-armenakas/ Email: ebookyab.ir@gmail.com, Phone:+989359542944 (Tetteram, WhatsApp, Eitaa)

(c) Referring to relation (1.61) the diagonal component of the tensor [B] in the direction

of the unit vector
$$\mathbf{i}_{n}$$
 is

$$B_{nn} = \left\{ n \right\}^{T} \left[B \right] \left\{ n \right\} = \frac{1}{\sqrt{3}} \left[1 \cdot 1 - 1 \right] \left[\begin{array}{c} 0 & 0 & 0 \\ 0 & 3 & -1 \\ 0 & -1 & 2 \end{array} \right] \left[\begin{array}{c} 1 \\ 1 \\ -1 \end{array} \right] \frac{1}{\sqrt{3}} = \frac{7}{3}$$

Problem 1.8C

Given the symmetric tensor of the second rank

$$\begin{bmatrix} c \end{bmatrix} = \begin{bmatrix} 2 & 0 & -3 \\ 0 & 0 & 0 \\ -3 & 0 & 4 \end{bmatrix}$$

(a) Referring to relation (1.124) we have the following stationary values for the tensor C

$$\widetilde{C}_{3} = \frac{1}{2} \left(\left(\frac{1}{33} + C_{11} \right) + \left\| \left(\frac{C_{33} - C_{11}}{2} \right)^{2} + C_{13}^{2} \right\|_{2}^{2} = 3 + 100$$

$$\widetilde{C}_{1} = \frac{1}{2} \left(\left(\frac{1}{33} + C_{11} \right) - \sqrt{\left(\frac{C_{33} - C_{11}}{2} \right)^{2} + C_{13}^{2}} = 3 - \sqrt{100}$$

$$\widetilde{C}_{2} = 0$$

From relation (1.122) we have

$$\tan 2\tilde{\phi}_{33} = \frac{2C_{13}}{C_{33} - C_{11}} = \frac{-6}{4 - 2} = -3 \text{ and } 2\tilde{\phi}_{33} = -71.56^\circ$$

Or

 $\overline{\phi}_{33} = 35.48^{\circ}$ clockwise

In Figure a, we show the principal axes \tilde{x}_3 , \tilde{x}_1



Figure a

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(b) Referring to relation (1.129) the maximum value of the non-diagonal components of

the tensor [C] is

$$\begin{pmatrix} C_{13} \end{pmatrix}_{max} = \left[\left(\frac{C_{33} - C_{11}}{2} \right)^2 + C_{13}^2 \right]^{1/2} = \left[1^2 + (-3)^2 \right]^{1/2} = \sqrt{10}$$
From relation (1.127) we have

$$\tan 2 \tilde{\phi}_{33} = -\frac{C_{33} - C_{11}}{2 C_{13}} = \frac{1}{3} \qquad \text{and} \quad 2 \tilde{\phi}_{33} = \sqrt{18} \cdot 43^\circ$$
Or

$$\tilde{\phi}_{33} = 9.22^\circ \qquad \text{counter-clockwise}$$
In Fig. a we show also the axes \tilde{x}_1, \tilde{x}_1 with respect of which this maximum value of the

non-diagonal components occurs.

(c) Referring to relation (1.61) the diagonal component of the tensor [C] in the direction of the unit vector \mathbf{i}_n is

$$C_{nn} = \left\{ n \right\}^{T} \left[C \right] \left\{ n \right\} = \frac{1}{13} \begin{bmatrix} 1 & 1 & -1 \end{bmatrix} \begin{bmatrix} 2 & 0 & -3 \\ 0 & 0 & 0 \\ -3 & 0 & 4 \end{bmatrix} \begin{bmatrix} 1 \\ -1 \\ -1 \end{bmatrix} \frac{1}{13} = \frac{12}{13} = 4$$

Problem 1.9 A

Given the symmetric tensor of the second rank

$$\begin{bmatrix} A \end{bmatrix} = \begin{bmatrix} -3 & -2 & 0 \\ -2 & 2 & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

(a) We plot Mohr's circle using the two points on the same diameter X_1 (-3, -2) and X_2 (2, 2). Referring to Figure a. we see that the center, C, of the circle is located on the A'₁₁ axis at a distance 1/2 (A₁₁ + A₂₂) = -0.5 from the origin O.



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From geometric considerations the radius, R, of the circle is

 $R = [(2.5)^2 + 2^2]^{1/2} = 3.2$

Moreover as shown in Fig. a the maximum value of the diagonal components of the tensor [A] is the abscissa of point \widetilde{X}_1 , while the minimum value is the abscissa of point \widetilde{X}_2 . Thus

$$(\vec{A}_{11})_{max} = \vec{A}_1 = \vec{C} \cdot \vec{X}_1 - \vec{OC} = 3.2 - 0.5 = 2.7$$

 $(\vec{A}_{11})_{min} = \vec{A}_2 = -(\vec{OC} + \vec{C} \cdot \vec{X}_2) = -3.2 - 0.5 = -3.7$

Referring to Fig. a. we have

$$\tan 2\widetilde{\varphi}_{11} = \tan < X_1 C \widetilde{X}_1 = 2/2.5$$

Hence

 $2\widetilde{\phi}_{11} = 218.66^\circ$ or $\widetilde{\phi}_{11} = 109.33^\circ$ counter- clockwise.

One of the principal directions is the i_3 whereas the other two lie in the x_1x_2 plane. So we see in Fig. a that point \tilde{X}_1 is located 218.66° clockwise from point X_1 . Consequently, the principal axis \tilde{x}_1 associated with the principal value \tilde{A}_1 of the diagonal component of the tensor is located $\tilde{\phi}_{11} = 109.33$ ° counter- clockwise from the x_1 axis. In Fig. b. we show the principal axes of the tensor \tilde{x}_1 , \tilde{x}_2 .



Figure b

(b) Referring to Fig. a the maximum non-diagonal component of the tensor is the ordinate of point \tilde{X}_1 . Thus,

$$(A_{12})_{max} = 3.2$$

From Fig. a we can see also that the point \tilde{X}_1 is located 128.66 ° clockwise from point X_1 . Consequently, the axes \tilde{x}_1 and \tilde{x}_2 , where the maximum value of the non-diagonal components of tensor [A] occur, are located as shown in Fig. b.

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(c) From relation (1.61) the diagonal component of the tensor [A] in the direction of the

vector
$$\mathbf{i}_{\mathbf{H}}$$
 is
 $A_{\mathbf{H}\mathbf{H}} = \left\{\mathbf{H}\right\}^{\mathsf{T}} \left[\mathbf{A}\right] \left\{\mathbf{H}\right\}^{\mathsf{T}} = \frac{1}{13} \begin{bmatrix} 1 & 1 & -1 \end{bmatrix} \begin{bmatrix} -3 & -2 & 0 \\ -2 & 2 & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 1 \\ 1 \\ -1 \end{bmatrix} \frac{1}{13} = -\frac{4}{3}$

Problem 1.9B

unit

Given the symmetric tensor of the second rank

$$\begin{bmatrix} 6 \end{bmatrix} = \begin{bmatrix} 6 & 0 & -3 \\ 0 & 0 & 0 \\ -3 & 0 & -2 \end{bmatrix}$$

(a) We plot Mohr's circle using the two points on the same diameter X_3 (-2, -3) and X_1 (6, 3). Referring to Figure a. we see that the center, C, of the circle is located on the B'₃₃ axis at a distance 1/2 (B₁₁ + B₂₂) = 2 from the origin O.



Figure a From geometric considerations the radius, R, of the circle is

$$R = (3^2 + 4^2)^{1/2} = 5$$

Moreover as shown in Fig. a the maximum value of the diagonal components of the tensor [B] is the abscissa of point \widetilde{X}_3 , while the minimum value is the abscissa of point \widetilde{X}_1 . Thus,

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$$(\mathbf{B}'_{33})_{\text{max}} = \widetilde{\mathbf{B}}_3 = \widetilde{\mathbf{CX}}_3 + \widetilde{\mathbf{OC}} = 5 + 2 = 7.0$$

 $(\mathbf{B}'_{11})_{\text{min}} = \widetilde{\mathbf{B}}_1 = -\widetilde{\mathbf{CX}}_1 + \widetilde{\mathbf{OC}} = -5 + 2 = -3.0$

Referring to Fig. a. we have

 $\tan 2\widetilde{\varphi_{33}} = \tan < X_3 \widetilde{CX_3} = 3/4$

Hence

 $2\widetilde{\varphi}_{33} = 216.87^{\circ}$ or $\widetilde{\varphi}_{33} = 108.43^{\circ}$ counter- clockwise.

One of the principal directions is the i_2 whereas the other two lie in the x_3x_1 plane. So we see in Fig. a that point \widetilde{X}_3 is located 216.87° clockwise from point X_3 . Consequently, the principal axis \widetilde{x}_3 associated with the principal value \widetilde{B}_3 of the diagonal component of the tensor is located $\widetilde{\phi}_{33} = 108.43$ ° counter- clockwise from the x_3 axis. In Fig. b. we show the principal axes of the tensor \widetilde{x}_3 , \widetilde{x}_1 .





(b) Referring to Fig. a the maximum non-diagonal component of the tensor is the ordinate of point X_3 . Thus,

 $(B'_{31})_{max} = 5$

From Fig. a we can also see that point \tilde{X}_3 is located 126.87 ° clockwise from point X_3 . Consequently, the axes \tilde{x}_3 and \tilde{x}_1 , where the maximum value of the non-diagonal components of tensor [B] occur, are located as shown in Fig. b.

(c) From relation (1.61) the diagonal component of the tensor [B] in the direction of the unit vector \mathbf{i}_n is $\mathbf{E}_{\mathbf{i}_n} = 2 \mathbf{I} \mathbf{E}_{\mathbf{i}_n}^{-1}$

$$B_{nn} = \{n\}^{T} [B] \{n\}^{2} = \frac{1}{13} [1 \ 1 \ -1] \begin{bmatrix} 6 \ 0 \ -3 \\ 0 \ 0 \ 0 \\ -3 \ 0 \ -2 \end{bmatrix} \begin{bmatrix} 1 \\ -1 \\ -1 \end{bmatrix} \frac{1}{13} = \frac{10}{3}$$

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Problem 1.9 C

Given the symmetric tensor of the second rank

$$\begin{bmatrix} C \end{bmatrix} = \begin{bmatrix} 0 & 0 & 0 \\ 0 & -2 & 4 \\ 0 & 4 & 6 \end{bmatrix}$$

(a) We plot Mohr's circle using the two points on the same diameter X_2 (-2, 4) and X_3 (6, -4). Referring to Figure a. we see that the center, C, of the circle is located on the C'₂₂ axis at a distance 1/2 (C₂₂ + C₃₃) = 2 from the origin O.



Figure a From geometric considerations the radius, R, of the circle is

 $R = (4^2 + 4^2)^{1/2} = 5.657$

Moreover as shown in Fig. a the maximum value of the diagonal components of the tensor [C] is the abscissa of point \widetilde{X}_2 , while the minimum value is the abscissa of point \widetilde{X}_3 . Thus

$$(C'_{22})_{max} = \widetilde{C}_2 = \widetilde{OC} + \widetilde{CX}_2 = 5.657 + 2 = 7.657$$

 $(C'_{22})_{min} = \widetilde{C}_3 = -\widetilde{CX}_3 + \widetilde{OC} = -5.657 + 2 = -3.657$

Referring to Fig. a. we have

 $2\widetilde{\phi}_{22} = \text{angle } X_2 C \widetilde{X}_2$

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Hence

 $2\tilde{\varphi}_{22} = 135^{\circ}$ or $\tilde{\varphi}_{22} = 67.5^{\circ}$ counter-clockwise.

One of the principal directions is the i_1 whereas the other two lie in the x_2x_3 plane. So we see in Fig. a that point \tilde{X}_2 is located 135° clockwise from point X_2 . Consequently, the principal axis \tilde{x}_2 associated with the principal value \tilde{C}_2 of the diagonal component of the tensor is located $\tilde{\phi}_{22} = 67.5$ ° counter-clockwise from the x_2 axis. In Fig. b. we show the principal axes of the tensor \tilde{x}_2 , \tilde{x}_3 .





(b) Referring to Fig. a the maximum non-diagonal component of the tensor is the ordinate of point X_2 . Thus,

 $(C'_{13})_{max} = 5.657$

From Fig. a we can also see that point \overline{X}_2 is located 45° clockwise from point X_2 . Consequently, the axes \overline{x}_2 and \overline{x}_3 , where the maximum value of the non-diagonal components of tensor [C] occur, are located as shown in Fig. b.

(c) From relation (1.61) the diagonal component of the tensor [C] in the direction of the unit vector i_n is

$$C_{mn} = \{n\} [c] \{n\} = \frac{1}{13} [1 \ 1 - 1] \begin{bmatrix} 0 & 0 & 0 \\ 0 & -2 & 4 \\ 0 & 4 & 6 \end{bmatrix} \begin{bmatrix} 1 \\ -1 \\ -1 \end{bmatrix} \frac{1}{13} = -\frac{4}{3}$$

Problem 1.9D

Given the symmetric tensor of the second rank

$$\begin{bmatrix} D \end{bmatrix} = \begin{bmatrix} -4 & 2 & 0 \\ 2 & -8 & 0 \\ 0 & 0 & 0 \end{bmatrix}$$

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(a) We plot Mohr's circle using the two points on the same diameter X_1 (-4, 2) and X_2 (-8, -2). Referring to Figure a. we see that the center, C, of the circle is located on the D'₁₁ axis at a distance 1/2 (D₁₁ + D₂₂) = -6 from the origin O.



From geometric considerations the radius, R, of the circle is

 $R = [2^2 + (-2)^2]^{1/2} = 2.828$

Moreover as shown in Fig. a the maximum value of the diagonal components of the tensor [D] is the abscissa of point X_1 , while the minimum value is the abscissa of point X_2 . Thus

$$(D'_{11})_{max} = \widetilde{D}_1 = -\widetilde{CO} + \widetilde{CX}_1 = -6 + 2.828 = -3.172$$

 $(D'_{11})_{min} = \widetilde{D}_2 = -\widetilde{CO} - \widetilde{CX}_2 = -6 - 2.828 = -8.828$

Referring to Fig. a. we have

 $\tan 2\widetilde{\phi}_{11} = \tan < X_i C \widetilde{X}_i = 1$

Hence

$$2\widetilde{\phi}_{11} = 45^{\circ}$$
 or $\widetilde{\phi}_{11} = 22.5^{\circ}$ counter clockwise.

One of the principal directions is the i_3 whereas the other two lie in the x_1x_2 plane. So we see in Fig. a that point \widetilde{X}_1 is located 45° clockwise from point X_1 . Consequently, the principal axis \widetilde{x}_1 associated with the principal value \widetilde{D}_1 of the diagonal component of the tensor is located $\widetilde{\phi}_{11} = 22.5$ ° counter- clockwise from the x_1 axis. In Fig. b we show the principal axes of the tensor \widetilde{x}_1 , \widetilde{x}_2 .

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(b) Referring to Fig. a the maximum non-diagonal component of the tensor is the ordinate of point X_1 . Thus,

 $(D'_{12})_{max} = 2.828$

From Fig. a we can see also that the point \tilde{X}_1 is located 45° clockwise from point X_1 . Consequently, the axes \tilde{X}_1 and \tilde{X}_2 , where the maximum value of the non-diagonal components of tensor [D] occur, are located as shown in Fig. b.

(c) From relation (1.61) the diagonal component of the tensor [D] in the direction of the unit vector \mathbf{i}_n is

$$D_{\eta\eta} = \{ n \}^{T} [D] \{ \eta \} = \frac{1}{13} [1 + 1] \begin{bmatrix} -4 & 2 & 0 \\ 2 & -8 & 0 \\ 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} 1 \\ 1 \\ 1 \\ 13 \end{bmatrix} = -\frac{8}{3}$$

Problem 1.9E

Given the symmetric tensor of the second rank

$$E = \begin{bmatrix} 0 & 3 & 0 \\ 3 & -9 & 0 \\ 0 & 0 & 2 \end{bmatrix}$$

(a) We plot Mohr's circle using the two points on the same diameter X_1 (0, 3) and X_2 (-9, -3). Referring to Figure a. we see that the center, C, of the circle is located on the E'₁₁ axis at a distance 1/2 (E₁₁ + E₂₂) = -4.5 from the origin O. From geometric considerations the radius, R, of the circle is

$$\mathbf{R} = [3^2 + (-4.5)^2]^{1/2} = 5.41$$

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As shown in Fig. a the maximum value of the diagonal components of the tensor [E] is the abscissa of point \widetilde{X}_1 , while the minimum value is the abscissa of point \widetilde{X}_2 . Thus

$$(\vec{E}'_{11})_{max} = \vec{E}_1 = \vec{C}\vec{X}_1 - \vec{CO} = 5.41 - 4.5 = 0.91$$

 $(\vec{E}'_{11})_{min} = \vec{E}_2 = -\vec{CO} - \vec{C}\vec{X}_2 = -4.5 - 5.41 = -9.91$

Referring to Fig. a. we have

 $\tan 2\tilde{\varphi}_{11} = \tan < X_1 C \tilde{X}_1 = 3/4.5$

Hence, $2\overline{\varphi}_{11} = 33.69^{\circ}$ or $\overline{\varphi}_{11} = 16.85^{\circ}$ counter clockwise.

One of the principal directions is the i_3 whereas the other two lie in the x_1x_2 plane. So we see in Fig. a that point \tilde{X}_1 is located 33.69° clockwise from point X_1 . Consequently, the principal axis \tilde{x}_1 associated with the principal value \tilde{E}_1 of the diagonal component of the tensor is located $\tilde{\varphi}_{11} = 16.85$ ° counter- clockwise from the x_1 axis. In Fig. b. we show the principal axes of the tensor \tilde{x}_1, \tilde{x}_2 .

(b) Referring to Fig. a the maximum non-diagonal component of the tensor is the ordinate of point \tilde{X}_{1} . Thus,

 $(E'_{12})_{max} = 5.41$

From Fig. a we also can see that the point \tilde{X}_1 is located 56.31° counter-clockwise from point X₁. Consequently, the axes \tilde{x}_1 and \tilde{x}_2 , where the maximum value of the non-diagonal components of tensor [E] occur, are located as shown in Fig. b.



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(c) From relation (1.61) the diagonal component of the tensor [E] in the direction of the unit vector $\mathbf{i}_{\mathbf{a}}$ is $\mathbf{a}_{\mathbf{b}} = \mathbf{a}_{\mathbf{b}} \mathbf{a}_{\mathbf{b}}$

$$E_{nn} = \{n\}^{T} [E] \{n\} = \frac{1}{\sqrt{3}} \begin{bmatrix} 1 & 1 & -1 \end{bmatrix} \begin{bmatrix} 0 & 3 & 0 \\ 3 & -9 & 0 \\ 0 & 0 & 2 \end{bmatrix} \begin{bmatrix} 1 \\ -1 \\ -1 \end{bmatrix}$$

Problem 1.9F

Given the symmetric tensor of the second rank

$$[F] = \begin{bmatrix} 0 & 0 & 0 \\ 0 & -4 & -3 \\ 0 & -3 & -12 \end{bmatrix}$$

(a) We plot Mohr's circle using the two points on the same diameter X_2 (-4, -3) and X_3 (-12, 3). Referring to Figure a we see that the center, C, of the circle is located on the F'₂₂ axis at a distance 1/2 (F₂₂ + F₃₃) = -8 from the origin O.

From geometric considerations the radius, R, of the circle is

 $\mathbf{R} = \left[(-3)^2 + (-4)^2 \right]^{1/2} = 5$

Moreover as shown in Fig. a the maximum value of the diagonal components of the tensor [F] is the abscissa of point \widetilde{X}_2 , while the minimum value is the abscissa of point \widetilde{X}_3 . Thus

$$(\mathbf{F}'_{22})_{\max} = \mathbf{\widetilde{F}}_2 = -\mathbf{\widetilde{CO}} + \mathbf{\widetilde{CX}}_2 = -\mathbf{8} + 5 = -3$$
$$(\mathbf{F}'_{22})_{\min} = \mathbf{\widetilde{F}}_3 = -\mathbf{\widetilde{CX}}_3 - \mathbf{\widetilde{CO}} = -5 - \mathbf{8} = -13$$

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Referring to Fig. a. we have

 $\tan 2\widetilde{\varphi}_{22} = \tan < X_2 C \widetilde{X}_2 = 3/4$

Hence

 $2\tilde{\phi}_{22} = 36.87^{\circ}$ or $\tilde{\phi}_{22} = 18.43^{\circ}$ clockwise.

One of the principal directions is the i_1 whereas the other two lie in the x_2x_3 plane. So we see in Fig. a that point \tilde{X}_2 is located 36.87° counter-clockwise from point X_2 . Consequently, the principal axis \tilde{x}_2 associated with the principal value \tilde{F}_2 of the diagonal component of the tensor is located $\tilde{\phi}_{22} = 18.43$ ° clockwise from the x_2 axis. In Fig. b. we show the principal axes of the tensor \tilde{x}_2, \tilde{x}_3 .



(b) Referring to Fig. a the maximum non-diagonal component of the tensor is the ordinate of point \widetilde{X}_2 . Thus,

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$(\mathbf{F}'_{23})_{\max} = 5.0$

From Fig. a we can also see that point \overline{X}_2 is located 126.87° counter-clockwise from point X_2 . Consequently, the axes \overline{x}_2 and \overline{x}_3 , where the maximum value of the non-diagonal components of tensor [C] occur, are located as shown in Fig. b.

(c) From relation (1.61) the diagonal component of the tensor [F] in the direction of the unit vector \mathbf{i}_{n} is -7.5

$$F_{nn} = \{n\}^{T} [F] \{n\} = \frac{1}{I_{3}} [1 \ 1 \ -1] \begin{bmatrix} 0 & 0 & 0 \\ 0 & -4 & -3 \\ 0 & -3 & -12 \end{bmatrix} \begin{bmatrix} 1 \\ 1 \\ 1 \\ \sqrt{3} \end{bmatrix} = -\frac{10}{3}$$

Problem 1.10A

Or

Referring to the solution of problem 1.9A we plot Mohr's circle in Fig. a. Moreover we plot line $X'_1CX'_2$ making an angle of 60° clockwise with line X_1CX_2 . Referring to Fig. a we have that

angle ACX'₁ = 21.34° and
A'₁₁ =
$$-\overline{OC} - \overline{CA} = -0.5 - R \cos(21.34°) = -3.481$$

A'₁₂ = $\overline{AX'_{1}} = R \sin(21.34°) = 3.2 \sin(21.34°) = 1.164$
A'₁₂ = $\overline{OB} = \overline{CB} - \overline{CO} = R \cos(21.34°) - 0.5 = 2.481$
[A'] = $\begin{bmatrix} -3.481 & 1.164 & 0\\ 1.164 & 2.481 & 0\\ 0 & 0 & 1 \end{bmatrix}$
A'₁₂ = $\overline{A_{11}} = \begin{bmatrix} -3.481 & 1.164 & 0\\ 1.164 & 2.481 & 0\\ 0 & 0 & 1 \end{bmatrix}$
A'₁₂ = $\overline{A_{11}} = \begin{bmatrix} -3.481 & 1.164 & 0\\ 1.164 & 2.481 & 0\\ 0 & 0 & 1 \end{bmatrix}$
A'₁₂ = $\overline{A_{12}} = \begin{bmatrix} -3.481 & 1.164 & 0\\ 1.164 & 2.481 & 0\\ 0 & 0 & 1 \end{bmatrix}$
A'₁₂ = $\overline{A_{12}} = \begin{bmatrix} -3.481 & 0\\ 1.164 & 2.481 & 0\\ 0 & 0 & 1 \end{bmatrix}$
A'₁₂ = $\overline{A_{12}} = \begin{bmatrix} -3.481 & 0\\ 1.164 & 2.481 & 0\\ 0 & 0 & 1 \end{bmatrix}$
A'₁₂ = $\overline{A_{12}} = \begin{bmatrix} -3.481 & 0\\ 1.164 & 2.481 & 0\\ 0 & 0 & 1 \end{bmatrix}$
A'₁₂ = $\overline{A_{12}} = \begin{bmatrix} -3.481 & 0\\ -2.481 & 0\\ 0 & 0 & 1 \end{bmatrix}$
A'₁₂ = $\overline{A_{12}} = \begin{bmatrix} -3.481 & 0\\ -2.481 & 0\\ 0 & 0 & 1 \end{bmatrix}$
A'₁₂ = $\overline{A_{12}} = \begin{bmatrix} -3.481 & 0\\ -2.481 & 0\\$

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Problem 1.10B

Referring to the solution of problem 1.9B we plot Mohr's circle in Fig. a. Moreover we plot line $X'_3CX'_1$ making an angle of 60° clockwise with line X_3CX_1 . Referring to Fig. a we have that



Problem 1.10D

Referring to the solution of problem 1.9D we plot Mohr's circle in Fig. a. Moreover we plot line $X'_1CX'_2$ making an angle of 60° clockwise with line X_1CX_2 . Referring to Fig. a we have that

angle $X'_1CA = 15^\circ$ and $D'_{11} = -\overline{CD} + R \cos(15^\circ) = -6 + 2.828 \cos(15^\circ) = -3.268$ $D'_{12} = -\overline{AX}'_1 = -R \sin(15^\circ) = -2.828 \sin(15^\circ) = -0.732$ $D'_{22} = -\overline{BD} = -(\overline{CO} + \overline{CB}) = -6 - R \cos(15^\circ) = -8.732$ https://ebookyab.ir/solution-manual-advanced-mechanics-of-materials-and-applied-elasticity-armenakas/ Email: ebookyab.ir@gmail.com, Phone:+989359542944 (Te**dagrea**m,**25**VhatsApp, Eitaa)



Figure a

Problem 1.10E

Referring to the solution of problem 1.9E we plot Mohr's circle in Fig. a. Moreover we plot line $X'_1CX'_2$ making an angle of 60° clockwise with line X_1CX_2 . Referring to Fig. a we have that

Or

Or

$$\begin{bmatrix} E' \end{bmatrix} = \begin{bmatrix} 0.35 & -2.40 & 0 \\ -2.40 & -9.35 & 0 \\ 0 & 0 & 2 \end{bmatrix}$$

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Figure a

Problem 1.11A

Given the symmetric tensor of the second rank

$$\begin{bmatrix} A \end{bmatrix} = \begin{bmatrix} 3 & -2 & 0 \\ -2 & 2 & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

Referring to relation (1.73a) we have

$$\begin{bmatrix} A' \end{bmatrix} = \begin{bmatrix} \Lambda_{s} \end{bmatrix} \begin{bmatrix} A \end{bmatrix} \begin{bmatrix} \Lambda_{s} \end{bmatrix}^{T}$$

$$= \begin{bmatrix} 1 & 0 & 0 \\ 0 & \frac{13}{2} & \frac{1}{2} \\ 0 & -\frac{1}{2} & \frac{13}{2} \end{bmatrix} \begin{bmatrix} 3 & -2 & 0 \\ -2 & 2 & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 & 0 \\ 0 & \frac{13}{2} & -\frac{1}{2} \\ 0 & \frac{1}{2} & \frac{13}{2} \end{bmatrix}$$

$$= \frac{1}{4} \begin{bmatrix} -12 & -413 & 4 \\ -413 & 4 & -13 \\ 4 & -13 & 5 \end{bmatrix}$$

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Problem 1.11E

Given the symmetric tensor of the second rank

$$\begin{bmatrix} \mathbf{F} \end{bmatrix} = \begin{bmatrix} 0 & 3 & 0 \\ 3 & -9 & 0 \\ 0 & 0 & 2 \end{bmatrix}$$

Referring to relation (1.73a) we have
$$\begin{bmatrix} \mathbf{E}' \end{bmatrix} = \begin{bmatrix} \Lambda_{1} \end{bmatrix} \begin{bmatrix} \mathbf{E} \end{bmatrix} \begin{bmatrix} \Lambda_{2} \end{bmatrix}^{T}$$
$$= \begin{bmatrix} \mathbf{i} & 0 & 0 \\ 0 & \frac{\mathbf{F}_{2}}{2} & \frac{1}{2} \\ 0 & -\frac{1}{2} & \frac{\mathbf{F}_{2}}{2} \end{bmatrix} \begin{bmatrix} 0 & 3 & 0 \\ 3 & -9 & 0 \\ 0 & 0 & 2 \end{bmatrix} \begin{bmatrix} \mathbf{i} & 0 & 0 \\ 0 & \frac{\mathbf{F}_{2}}{2} & -\frac{1}{2} \\ 0 & \frac{1}{2} & \frac{\mathbf{F}_{2}}{2} \end{bmatrix}$$
$$= \frac{1}{4} \begin{bmatrix} 0 & 6\mathbf{F}_{2} & -6 \\ 6\mathbf{F}_{3} & -2\mathbf{S} & \mathbf{H}\mathbf{F}_{3} \\ -6 & \mathbf{H}\mathbf{F}_{3} & -3 \end{bmatrix}$$

Problem 1.12

The state of stress of the particle of Fig. 1P12 is

$$\begin{bmatrix} 60 & 0 & 30 \\ 0 & 0 & 0 \\ 30 & 0 & -20 \end{bmatrix}$$

(a) The unit vector \mathbf{i}_s normal to \mathbf{i}_n , which lies in the x_1 , x_3 plane, is

$$\frac{1}{5} = \frac{4}{5}\frac{1}{5} - \frac{3}{5}\frac{1}{5}\frac{3}{5}$$

Thus referring to relation (1.61) we have

$$z_{nn} = \{n\}^{T} [\tau] \{n\} = \frac{1}{5} [3 \circ 4] \begin{bmatrix} 60 & 0 & 30 \\ 0 & 0 & 0 \\ 30 & 0 & -20 \end{bmatrix} \begin{bmatrix} 3 \\ 0 \\ 4 \end{bmatrix} = 31.6 \text{ MPa}$$

Referring to relation (1.64a) we have

$$\tau_{ns} = \{n\}^{T} [\tau] \{s\} = \frac{1}{5} [3 \circ 4] \begin{bmatrix} 60 & 0 & 30 \\ 0 & 0 & 0 \\ 30 & 0 & -20 \end{bmatrix} \begin{bmatrix} 4 \\ 0 \\ -3 \end{bmatrix} = 46.80 \text{ MPa}$$

The positive sign indicates that τ_{ns} is in the direction of the unit vector is as we show in Fig. a.



Figure a Results

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Another way of solving this problem is using Mohr's circle. We plot the circle using two points X_3 (-20, 30) and X_1 (60, -30). These points are located on the same diameter of the circle. Referring to Fig. b we see that the center, C of the circle is located on the τ'_{33} axis at a distance $\overline{OC} = 1/2 (\tau_{33} + \tau_{11}) = 20$ from the origin O. From geometric considerations we have also that the radius of the circle is



The point of Mohr's circle whose coordinates are the components of stress acting on the plane normal to the unit vector i_n , referring to Fig. c, is located $2x36.87^\circ = 73.74^\circ$ clockwise from point X_3 .



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Thus, referring to Fig. b, we have that

 $\tau_{nn} = \widetilde{OC} + \widetilde{CD} = 20 + R \cos(69.39^{\circ}) = 37.6 \text{ MPa}$ $\tau_{ns} = R \sin(69.39^{\circ}) = 46.80 \text{ MPa}$

(b) Referring to Fig. b we see that the maximum normal component of stress is the abscissa of point \widetilde{X}_3 . Thus,

and

 $(\tau'_{33})_{max} = \overrightarrow{OC} + R = 20 + 50 = 70 \text{ MPa}$

Moreover, $\tan 2\widetilde{\varphi}_{33} = -30 / 40 = -0.75$

 $2\widetilde{\varphi}_{33} = 143.14^{\circ}$ or $\widetilde{\varphi}_{33} = 71.57^{\circ}$ counter -clockwise

In Fig. d we show the plane on which the maximum normal component of stress acts.



Figure d Principal directions & maximum component of stress

(c) The maximum shearing component of stress is the ordinate of point \tilde{X}_3 . Thus,

 $(\tau'_{31})_{max} = R = 50 \text{ MPa}$ Moreover $\langle X_3 C \widetilde{X}_3 = 143.14^\circ - 90^\circ = 53.14^\circ \text{ and } \widetilde{\phi}_{33} = 26.57^\circ \text{ counter - clockwise}$ In Fig. e we show the plane on which the maximum shearing component of stress acts.



Figure e Plane of maximum shear stress

(d) Referring to relation (1.61) the normal component of stress acting on the plane normal to unit vector $i_n = 1/3$ ($i_1 - i_2 + i_3$) is

$$z_{nn} = \{n\}^{T} [z] \{n\} = \frac{1}{I_{3}} [1 - 1 + 1] \begin{bmatrix} 60 & 0 & 30 \\ 0 & 0 & 0 \\ 30 & 0 & -20 \end{bmatrix} \begin{bmatrix} 1 \\ -1 \\ 1 \end{bmatrix} \frac{1}{I_{3}} = \frac{100}{3} \text{ MPa}$$

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Problem 1.13

The state of stress of the particle of Fig. 1P13 is

$$\begin{bmatrix} z \end{bmatrix} = \begin{bmatrix} -120 & 0 & -30 \\ 0 & 0 & 0 \\ -30 & 0 & -40 \end{bmatrix}$$

(a) The unit vector \mathbf{i}_s normal to \mathbf{i}_n , which lies in the x_1 , x_3 plane, is

$$i_{5} = \frac{4}{5}i_{1} - \frac{3}{5}i_{3}$$

Thus referring to relation (1.61) we have

$$z_{\eta\eta} = \{\eta\}^{T} [z] \{\eta\} = \frac{1}{5} [3 \circ 4] \begin{bmatrix} -120 \circ -30 \\ 0 \circ 0 \end{bmatrix} \begin{bmatrix} 3 \\ 0 \\ -30 \circ -40 \end{bmatrix} \begin{bmatrix} 3 \\ 4 \end{bmatrix} \frac{1}{5} = -97.6 \text{ MPa}$$

-

Referring to relation (1.64a) we have

$$z_{\eta_{s}} = \left\{n\right\}^{T} \left[\overline{c}\right] \left\{s\right\} = \frac{1}{5} \left[3 \circ 4\right] \left[-\frac{120 \circ -30}{0 \circ 0} -\frac{1}{5}\right] \left[\frac{4}{0}\right] \frac{1}{5} = -46.8 \text{ MPa}$$

The negative sign indicates that τ_{ns} is in the opposite direction of the unit vector i_s . That is as we show in Fig. a.



Figure a Results

Another way of solving this problem is using Mohr's circle. We plot the circle using two points X_3 (-40, -30) and X_1 (-120, 30). These points are located on the same diameter of the circle. Referring to Fig. b we see that the center, C of the circle is located on the τ_{33} axis at a distance 1/2 ($\tau_{33} + \tau_{11}$) = -80 from the origin O. From geometric considerations we have also that the radius of the circle is

 $R = (40^2 + 30^2)^{1/2} = 50$

The point of Mohr's circle whose coordinates are the components of stress acting on the plane normal to the unit vector i_n , which referring to Fig. c of the solution of problem 1.12, is located $2x36.87^\circ = 73.74^\circ$ clockwise from point X₃. So from Fig. b we have that

 $2nn = -(\overline{OC} + \overline{CO}) = -[80 + R\cos(63.39^{\circ})] = -97.60 \text{ MPa}$ $2ns = -R\sin(69.39^{\circ}) = -46.80 \text{ MPa}$ https://ebookyab.ir/solution-manual-advanced-mechanics-of-materials-and-applied-elasticity-armenakas/ Email: ebookyab.ir@gmail.com, Phone:+989359542944 (T@lageram31WhatsApp, Eitaa)



Figure b Mohr's circle

(b) Referring to Fig. b we have that the maximum normal component of stress is the abscissa of point X'_3 . Thus

(13) max = - 20+R = - 80+50 = - 30 MPa

In following Fig. c we show the plane on which it acts



Figure c Principal directions & maximum component of stress

(c) The maximum shearing component of stress is the ordinate of point X_3 . Thus $(\tau'_{31})_{max} = 50 \text{ M/Pa}$

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In Fig. d we show the plane on which the maximum shearing component of stress acts



Figure d Plane of maximum shear stress

(d) Referring to relation (1.61) the normal component of stress acting on the plane normal to unit vector $i_n = 1/3$ ($i_1 - i_2 + i_3$) is

$$\tau_{n\eta} = \left\{ n \right\}^{T} \left[z \right] \left\{ n \right\} = \frac{1}{13} \begin{bmatrix} 1 - 1 & 1 \end{bmatrix} \begin{bmatrix} -120 & 0 & -30 \\ 0 & 0 & 0 \\ -30 & 0 & -40 \end{bmatrix} \begin{bmatrix} 1 \\ -1 \\ 1 \end{bmatrix} \frac{1}{13} = \frac{220}{3}$$

Problem 1.14

(a) Referring to relations (1.78) to (1.80) the invariants of the tensor [A] are

 $II_1 = 3$ $II_2 = -21$ $II_3 = 4$

Thus, relation (1.105) becomes

$$A_{K}^{3} - 3A_{K}^{2} - 21A_{K} - 4 = 0$$

The roots of this equation are

Substituting $A_1 = 6.3863$ into the first two of relations (1.103) we obtain

$$(3-6.3863)\lambda_{11}^{(i)} + 4\lambda_{12}^{(i)} + \lambda_{13}^{(i)} = 0$$

 $4\lambda_{11}^{(i)} + (0-6.3863)\lambda_{12}^{(i)} + 2\lambda_{13}^{(i)} = 0$

Thus,

$$\lambda_{12}^{(i)} = 0.7488 \ \lambda_{11}^{(i)}$$

$$\lambda_{13}^{(i)} = 0.3911 \ \lambda_{11}^{(i)}$$
(a)

Referring to equation (1.96), from the orthogonality condition $i_1^{(1)}$, $i_1^{(1)} = 1$ we have

$$(\lambda_{11}^{(0)})^{2} + (\lambda_{12}^{(0)})^{2} + (\lambda_{13}^{(0)})^{2} = 1$$
 (b)

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Solving relations (a) and (b) we get

 $\lambda_{11}^{(1)} = \pm 0.7639$ $\lambda_{12}^{(1)} = \pm 0.5720$ $\lambda_{13}^{(1)} = \pm 0.2988$

The set of direction cosines with the upper sign specifies the same direction as the set of

direction cosines with the lower sign but opposite sense.

Substituting $A_2 = -0.1963$ into the first of relations (1.103) we get $(3+0.1963) \lambda_{21}^{(2)} + 4 \lambda_{22}^{(2)} + \lambda_{23}^{(2)} = 0$ $4 \lambda_{21}^{(2)} + 0.1963 \lambda_{22}^{(2)} + 2 \lambda_{23}^{(2)} = 0$ Thus, $\lambda_{22}^{(2)} = -0.3066 \lambda_{21}^{(2)}$ (c) $\lambda_{23}^{(2)} = -1.9699 \lambda_{21}^{(2)}$

and

$$(\lambda_{21}^{(2)})^2 + (\lambda_{22}^{(2)})^2 + (\lambda_{23}^{(2)})^2 = 1$$
 (d)

Solving relations (c) and (d) we have $\lambda_{21}^{(2)} = \pm 0.4484$ $\lambda_{22}^{(2)} = \mp 0.1375$ $\lambda_{23}^{(2)} = \mp 0.8833$

Substituting $A_3 = -3.19$ into the first two of relations (1.103) we have

$$(3+3.19) \lambda_{31}^{(3)} + 4 \lambda_{32}^{(3)} + \lambda_{33}^{(3)} = 0$$

$$4 \lambda_{31}^{(3)} + 3.19 \lambda_{32}^{(3)} + 2 \lambda_{33}^{(3)} = 0$$

Thus,

$$\lambda_{32}^{(3)} = -1.7422 \ \lambda_{31}^{(3)}$$

$$\lambda_{33}^{(3)} = 0.7788 \ \lambda_{31}^{(3)}$$
(e)

and

$$(\lambda_{31}^{(3)})^2 + (\lambda_{32}^{(3)})^2 + (\lambda_{33}^{(3)})^2 = 1$$
 (f)

Solving relations (e) and (f) we get $\lambda_{31}^{(3)} = \pm 0.4641$ $\lambda_{32}^{(3)} = \mp 0.8086$ $\lambda_{33}^{(3)} = \pm 0.3614$

Thus, the principal directions of the tensor are

$$\tilde{i}_{1}^{(1)} = 0.7639 \underline{i}_{1} + 0.5720 \underline{i}_{2} + 0.2988 \underline{i}_{3}$$

$$\tilde{i}_{2}^{(2)} = 0.4484 \underline{i}_{1} - 0.1375 \underline{i}_{2} - 0.8833 \underline{i}_{3}$$

$$\tilde{i}_{3}^{(3)} = 0.4641 \underline{i}_{1} - 0.8086 \underline{i}_{2} + 0.3614 \underline{i}_{3}$$
(g)

As a check we apply the orthogonality conditions $i_1^{(1)}$. $i_2^{(2)} = 0$ and $i_1^{(1)}$. $i_3^{(3)} = 0$.

Referring to relations (1.25a) we have

 $\lambda_{11}^{(1)} \ \lambda_{12}^{(2)} + \lambda_{21}^{(1)} \ \lambda_{22}^{(2)} + \lambda_{31}^{(1)} \ \lambda_{32}^{(2)} = 0$ $\lambda_{11}^{(1)} \lambda_{13}^{(3)} + \lambda_{21}^{(1)} \lambda_{23}^{(3)} + \lambda_{31}^{(1)} \lambda_{33}^{(3)} = 0$

or

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(b) Referring to relations (1.143) the maximum values of the non-diagonal components

$$(A'_{12})_{max} = \frac{A_1 - A_2}{2} = 3.2913$$

$$(A'_{13})_{max} = \frac{A_1 - A_3}{2} = 4.7882$$

$$(A'_{23})_{max} = \frac{A_2 - A_3}{2} = 1.4969$$

.

Problem 1.15

(a) Referring to relations (1.78) to (1.80) the invariants of the tensor [A] are

$$\Pi_{1}=7$$
 $\Pi_{2}=0$ $\Pi_{3}=-25$

Thus, relation (1.105) becomes

$$A_{k}^{3} - 7 A_{k}^{2} + 25 = 0$$

The roots of this equation are

$$A_1 = 6.3872$$
 $A_2 = 2.3084$ $A_3 = -1.6956$

Substituting $A_1 = 6.3872$ into the first two of relations (1.103) we obtain

$$(1-6.3872) \lambda_{11}^{(1)} - 2 \lambda_{12}^{(1)} + \lambda_{13}^{(1)} = 0$$

-2 $\lambda_{11}^{(1)} + (4-6.3872) \lambda_{12}^{(1)} + 3 \lambda_{13}^{(1)} = 0$

Thus,

$$\lambda_{12}^{(1)} = -3.9198 \lambda_{11}^{(1)}$$

$$\lambda_{13}^{(1)} = -2.4526 \lambda_{11}^{(1)}$$
(a)

Referring to equation (1.96), from the orthogonality condition $i_1^{(1)}$, $i_1^{(1)} = 1$ we have

$$(\lambda_{11}^{(1)})^2 + (\lambda_{12}^{(1)})^2 + (\lambda_{13}^{(1)})^2 = 1$$
 (b)

Solving relations (a) and (b) we get

$$\lambda_{11}^{(i)} = \pm 0.2114$$
 $\lambda_{12}^{(i)} = \mp 0.8285$ $\lambda_{13}^{(i)} = \mp 0.5185$

The set of direction cosines with the upper sign specifies the same direction as the set of direction cosines with the lower sign but opposite sense.

Substituting $A_2 = 2.3084$ into the first of relations (1.103) we get

$$(1-2.3084)\lambda_{21}^{(2)} - 2\lambda_{22}^{(2)} + \lambda_{23}^{(2)} = 0$$

-2 $\lambda_{21}^{(1)} + (4-2.3084)\lambda_{22}^{(2)} + 3\lambda_{23}^{(2)} = 0$

Thus,

$$\lambda_{22}^{(2)} = -0.2503 \lambda_{21}^{(2)}$$
(c)
$$\lambda_{23}^{(2)} = 0.8078 \lambda_{21}^{(2)}$$

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and

$$(\lambda_{21}^{(2)})^{2} + (\lambda_{22}^{(2)})^{2} + (\lambda_{23}^{(2)})^{2} = 1$$
(d)
Solving relations (c) and (d) we have

$$\lambda_{21}^{(2)} = \pm 0.7636 \quad \lambda_{22}^{(2)} = \pm 0.1911 \quad \lambda_{23}^{(2)} = \pm 0.6168$$
Substituting A₃ = -1.6956 into the first two of relations (1.103) we have

$$(1 + 1.6956)\lambda_{31}^{(3)} - 2\lambda_{32}^{(3)} + \lambda_{33}^{(3)} = 0$$

$$-2\lambda_{31}^{(3)} + (4 + 1.6956)\lambda_{32}^{(3)} + 3\lambda_{33}^{(3)} = 0$$

Thus,

$$\lambda_{32}^{(3)} = 0.8624 \ \lambda_{31}^{(3)}$$

$$\lambda_{33}^{(3)} = -0.9708 \ \lambda_{31}^{(3)}$$
(e)

and

$$(\lambda_{31}^{(3)})^2 + (\lambda_{32}^{(3)})^2 + (\lambda_{33}^{(3)})^2 = 1$$
 (f)

Solving relations (e) and (f) we get

$$\lambda_{31}^{(3)} = \pm 0.6101$$
 $\lambda_{32}^{(3)} = \pm 0.5262$ $\lambda_{33}^{(3)} = \pm 0.5923$

Thus, the principal directions of the tensor are

$$\tilde{i}_{1}^{(1)} = 0.2114 \underline{i}_{1} - 0.8285 \underline{i}_{2} - 0.5185 \underline{i}_{3}$$

$$\tilde{i}_{2}^{(2)} = 0.7636 \underline{i}_{1} - 0.1911 \underline{i}_{2} + 0.6168 \underline{i}_{3}$$

$$\tilde{i}_{3}^{(3)} = 0.6101 \underline{i}_{1} + 0.5262 \underline{i}_{2} - 0.5923 \underline{i}_{3}$$

(b) Referring to relations (1.143) the maximum values of the non-diagonal components of the tensor are

$$(A'_{12})_{max} = \frac{A_1 - A_2}{2} = 2.0394$$
$$(A'_{13})_{max} = \frac{A_1 - A_3}{2} = 4.0414$$
$$(A'_{23})_{max} = \frac{A_2 - A_3}{2} = 2.002$$

Problem 1.16

(a) Referring to relations (1.78) to (1.80) the invariants of the tensor are

$$\Pi_{1}=0$$
 $\Pi_{2}=-25$ $\Pi_{3}=0$

Thus, relation (1.105) becomes

$$A_{K}^{3} - 25A_{K} = 0$$

The roots of this equation are

 $A_{1=0}$ $A_{2}=5$ $A_{3}=-5$

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Substituting $A_1 = 0$ into the first two of relations (1.103) we obtain

$$4 \lambda_{12}^{(1)} + 3 \lambda_{13}^{(1)} = 0$$

$$4 \lambda_{11}^{(1)} = 0$$

Thus,

$$\lambda_{12}^{(1)} = -0.75 \lambda_{13}^{(1)}$$

$$\lambda_{11}^{(1)} = 0$$
(a)

Referring to equation (1.96), from the orthogonality condition $i_1^{(1)}$ $i_1^{(1)} = 1$ we have

$$(\lambda_{i_1}^{(i)})^2 + (\lambda_{i_2}^{(i)})^2 + (\lambda_{i_3}^{(i)})^2 = 1$$
 (b)

Solving relations (a) and (b) we get

$$\lambda_{11}^{(1)} = 0$$
 $\lambda_{12}^{(1)} = \mp \frac{3}{5}$ $\lambda_{13}^{(1)} = \pm \frac{4}{5}$

The set of direction cosines with the upper sign specifies the same direction as the set of direction cosines with the lower sign but opposite sense.

Substituting $A_2 = 5$ into the first of relations (1.103) we get

$$-5 \lambda_{21}^{(2)} + 4 \lambda_{22}^{(2)} + 3 \lambda_{23}^{(2)} = 0$$

$$4 \lambda_{21}^{(2)} - 5 \lambda_{22}^{(2)} = 0$$

$$\lambda_{21}^{(2)} = \frac{5}{4} \lambda_{22}^{(2)}$$

Thus,

$$\lambda_{21}^{(2)} = \frac{5}{4} \cdot \lambda_{22}^{(2)}$$

$$\lambda_{23}^{(2)} = \frac{3}{4} \cdot \lambda_{22}^{(2)}$$
(c)

and

$$(\lambda_{21}^{(2)})^2 + (\lambda_{22}^{(2)})^2 + (\lambda_{23}^{(2)})^2 = 1$$
 (d)

Solving relations (c) and (d) we have

$$\lambda_{21}^{(2)} = \pm \frac{1}{12}$$
 $\lambda_{22}^{(2)} = \pm \frac{4}{512}$ $\lambda_{23}^{(2)} = \pm \frac{3}{512}$

Substituting $A_3 = -5$ into the first two of relations (1.103) we have

$$5 \lambda_{3i}^{(3)} + 4 \lambda_{32}^{(3)} + 3 \lambda_{33}^{(3)} = 0$$

$$4 \lambda_{3i}^{(3)} + 5 \lambda_{32}^{(3)} = 0$$
Thus,
$$\lambda_{31}^{(3)} = -\frac{5}{4} \lambda_{32}^{(3)}$$
(e)
$$\lambda_{33}^{(3)} = \frac{3}{4} \lambda_{32}^{(3)}$$
and
$$(\lambda_{31}^{(3)})^{2} + (\lambda_{32}^{(3)})^{2} + (\lambda_{33}^{(3)})^{2} = 1$$
(f)

and

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Solving relations (e) and (f) we get

$$\lambda_{31}^{(3)} = -\frac{1}{12} \qquad \lambda_{32}^{(3)} = -\frac{4}{512} \qquad \lambda_{33}^{(3)} = \pm \frac{3}{512}$$
Thus, the principal directions of the tensor are
$$\tilde{i}_{1}^{(1)} = -\frac{3}{5} \cdot i_{2} + \frac{4}{5} \cdot i_{3}$$

$$\tilde{i}_{2}^{(2)} = \frac{1}{12} \cdot i_{1} + \frac{4}{512} \cdot i_{2} + \frac{3}{512} \cdot i_{3}$$

$$\tilde{i}_{3}^{(3)} = -\frac{1}{12} \cdot i_{1} + \frac{4}{512} \cdot i_{2} + \frac{3}{512} \cdot i_{3}$$
As a check we apply the orthogonality conditions $i_{1}^{(1)} \cdot i_{2}^{(2)} = 0$ and $i_{1}^{(1)} \cdot i_{3}^{(3)} = 0$.

Referring to relations (1.25a) we have

$$\lambda_{11}^{(1)} \lambda_{12}^{(2)} + \lambda_{21}^{(1)} \lambda_{22}^{(2)} + \lambda_{31}^{(1)} \lambda_{32}^{(2)} = 0$$

or

$$0 \cdot \frac{1}{12} - \frac{3}{5} \cdot \frac{4}{512} + \frac{4}{5} \cdot \frac{3}{512} = 0$$

$$0 \cdot \left(-\frac{1}{12}\right) - \frac{3}{5} \cdot \frac{4}{512} + \frac{4}{5} \cdot \frac{3}{512} = 0$$

(b) Referring to Fig. 1P16 the transformation matrix is

$$\begin{bmatrix} \Lambda_{S} \end{bmatrix} = \begin{bmatrix} 0.866 & 0.5 & 0 \\ -0.5 & 0.866 & 0 \\ 0 & 0 & 1 \end{bmatrix}$$
 (h)

Substituting (h) into relation (1.73a) we have

$$\begin{bmatrix} A' \end{bmatrix} = \begin{bmatrix} 0.866 & 0.5 & 0 \\ -0.5 & 0.866 & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 0 & 4 & 3 \\ 4 & 0 & 0 \\ 3 & 0 & 0 \end{bmatrix} \begin{bmatrix} 0.866 & -0.5 & 0 \\ 0.5 & 0.866 & 0 \\ 0 & 0 & 1 \end{bmatrix}$$
$$= \begin{bmatrix} 3.464 & 2 & 2.598 \\ 2 & -3.464 & -1.5 \\ 2.598 & -1.5 & 0 \end{bmatrix}$$