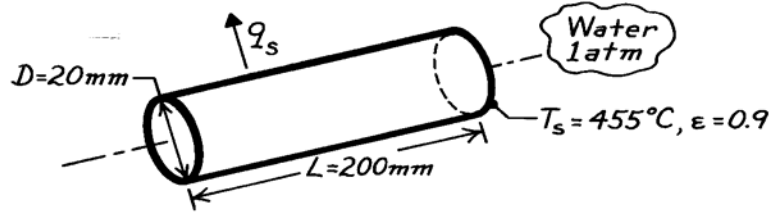


### PROBLEM 10.30

**KNOWN:** Steel bar upon removal from a furnace immersed in water bath.

**FIND:** Initial heat transfer rate from bar.

**SCHEMATIC:**



**ASSUMPTIONS:** (1) Uniform bar surface temperature, (2) Film pool boiling conditions.

**PROPERTIES:** Table A-6, Water, liquid (1 atm,  $T_{\text{sat}} = 100^\circ\text{C}$ ):  $\rho_\ell = 957.9 \text{ kg/m}^3$ ,  $h_{\text{fg}} = 2257 \text{ kJ/kg}$ ; Table A-4, Water, vapor ( $T_f = (T_s + T_{\text{sat}})/2 = 550\text{K}$ ):  $\rho_v = 0.4005 \text{ kg/m}^3$ ,  $c_{p,v} = 1997 \text{ J/kg}\cdot\text{K}$ ,  $\nu_v = 47.04 \times 10^{-6} \text{ m}^2/\text{s}$ ,  $k_v = 0.0379 \text{ W/m}\cdot\text{K}$ .

**ANALYSIS:** The total heat transfer rate from the bar at the instant of time it is removed from the furnace and immersed in the water is

$$q_s = \bar{h} A_s (T_s - T_{\text{sat}}) = \bar{h} A_s \Delta T_e \quad (1)$$

where  $\Delta T_e = 455 - 100 = 355\text{K}$ . According to the boiling curve of Figure 10.4, with such a high  $\Delta T_e$ , film pool boiling will occur. From Eq. 10.9 or 10.10,

$$\bar{h}^{4/3} = \bar{h}_{\text{conv}}^{4/3} + \bar{h}_{\text{rad}} \cdot \bar{h}^{1/3} \quad \text{or} \quad \bar{h} = \bar{h}_{\text{conv}} + \frac{3}{4} \bar{h}_{\text{rad}} \quad (\text{if } h_{\text{conv}} > h_{\text{rad}}). \quad (2)$$

To estimate the convection coefficient, use Eq. 10.8,

$$\text{Nu}_D = \frac{\bar{h}_{\text{conv}} D}{k_v} = C \left[ \frac{g(\rho_\ell - \rho_v) h'_{\text{fg}} D^3}{\nu_v k_v \Delta T_e} \right]^{1/4} \quad (3)$$

where  $C = 0.62$  for the horizontal cylinder and  $h'_{\text{fg}} = h_{\text{fg}} + 0.8 c_{p,v} (T_s - T_{\text{sat}})$ . Find

$$\bar{h}_{\text{conv}} = \frac{0.0379 \text{ W/m}\cdot\text{K}}{0.020 \text{ m}} \cdot 0.62 \left[ \frac{9.8 \text{ m/s}^2 (957.9 - 0.4005) \text{ kg/m}^3 \left[ 2257 \times 10^3 + 0.8 \times 1997 \times 355 \right] \text{ J/kg} (0.020 \text{ m})^3}{(47.04 \times 10^{-6}) \text{ m}^2/\text{s} \times 0.0379 \text{ W/m}\cdot\text{K} \times 355 \text{ K}} \right]^{1/4}$$

$$\bar{h}_{\text{conv}} = 159 \text{ W/m}^2 \cdot \text{K}.$$

To estimate the radiation coefficient, use Eq. 10.11,

$$\bar{h}_{\text{rad}} = \frac{\varepsilon \sigma (T_s^4 - T_{\text{sat}}^4)}{T_s - T_{\text{sat}}} = \frac{0.9 \times 5.67 \times 10^{-8} \text{ W/m}^2 \cdot \text{K}^4 (728^4 - 373^4) \text{ K}^4}{355 \text{ K}} = 37.6 \text{ W/m}^2 \cdot \text{K}.$$

Substituting numerical values into the simpler form of Eq. (2), find

$$\bar{h} = (159 + (3/4)37.6) \text{ W/m}^2 \cdot \text{K} = 187 \text{ W/m}^2 \cdot \text{K}.$$

Using Eq. (1), the heat rate, with  $A_s = \pi D L$ , is

$$q_s = 187 \text{ W/m}^2 \cdot \text{K} (\pi \times 0.020 \text{ m} \times 0.200 \text{ m}) \times 355 \text{ K} = 835 \text{ W}.$$

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**COMMENTS:** For these conditions, the combined radiation and convection heat transfer coefficient is 18% larger than the convection coefficient alone.